

Performance Analysis of Power System Indices for Islanding Detection

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Abstract

Objective: In this work, a passive islanding detection technique based on performance analysis of power system indices has been proposed for a hybrid system. **Method:** The commonly used 12 different power system indices are analyzed on the basis of sensitivity/performance under all possible islanding and non-islanding scenarios, such as capacitor injection/ejection, load increment/decrement, starting of induction motor, single and three phase faults. **Findings:** It has been found, based on performance analysis, that active power shows the highest capability to distinguish minute variations in the system. Subsequently, a passive technique, that utilizes active power as a discriminative feature, is proposed. Further, a protracted study is conducted to test the capability of the technique to discern the islanding and non-islanding scenarios of comparable signatures. **Application/improvements:** This technique presents high accuracy and zero impact on power quality. These characteristics make this technique appropriate for real-world operation.

Keywords: Power Indices, Islanding Detection, Performance Analysis, Distributed Generation, NDZ.

1. Introduction

The world is moving towards distributed energy resources (DERs) due to the prevailing global warming threat, a rapid decrease in world conventional energy resources and high transmission losses. These DERs are more reliable, cost-effective, sustainable and efficient to meet world energy needs. They grant many merits such as high-power quality, low carbon emission and minimize transmission and distribution (T&D) losses. The DERs consist of sustainable energy sources such as tidal, biomass, wind, solar, and fuel cell.¹

Besides the merits of integration of DERs with the power system, the dynamic behavior of these resources is the reason for several technical challenges. These challenges include failure of protection, incorrect tripping of feeder relay, islanding operational issue, loss of coordination, fault current locator and auto recloser

problems.^{2,3} The most significant challenge is known as “islanding”. In islanding condition, DERs keeps on supplying power to the load, despite the isolation of the utility from the system⁴⁻⁶ as demonstrated.

When the load supply from the utility grid is turned off, a virtual island is established as represented by the dotted rectangle in Figure 1. Islanding phenomena cause several complex situations such as instability of power system, poor power quality, life risks for the workers and equipment damage. To tackle the aforementioned concerns, power system standards such as IEC 62116, IEEE 929-2000, IEEE 1547-2007, AS4777.3-2005 suggested preventing stop DER operation during islanding conditions.^{4,7,8} IEEE 1547 standard states that islanding conditions should be recognized within 2 seconds and DERs should be isolated from the distribution network.⁹ For this purpose, many techniques have been established and each technique has its own favorable and unfavorable aspect.¹⁰

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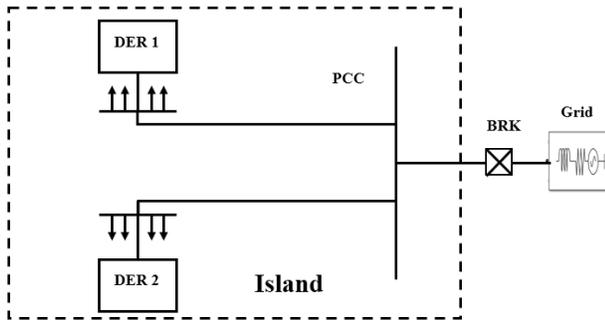


Figure 1. Islanding occurrence phenomenon.

At present, the islanding detection techniques are grouped as remote and local techniques.^{4,11,12} The remote techniques follow the principle of communication, and this communication occurs between the utility grid and DERs. Each DER has a receiver whereas, a circuit breaker connected to the utility grid has a transmitter. Whenever the utility grid is disconnected due to any disturbance, a signal is transmitted towards DER for immediate tripping. This technique has various positive characteristics such as high reliability, rapid detection time, negligible impact on power quality and zero non-detection zones (NDZ). This technique shows remarkable performance in the case of multiple DERs(4,10,13), due to is high installation and operational cost, it is not suitable for small systems. Phasor measurement unit (PMU), supervisory control and data acquisition system (SCADA),¹³ power line carrier communication (PLCC)(13), transfer tripping scheme (TTS) and impedance insertion come under the remote islanding techniques.¹⁴⁻¹⁷

In local techniques, system parameters are observed at the point of common coupling (PCC) and are further classified into three main categories such as active, passive and hybrid techniques.¹⁸ In active islanding detection method, the perturbations are fed to the system's local variables and these variables include frequency, current and voltage.¹⁸ The impact of this perturbation will be significant for islanding scenarios otherwise it will be minute. Researchers have proposed many active islanding detection methods such as, Sandia frequency shift (SFS),^{16,19,20} reactive power export error detection (RPEED),²¹ detection of impedance at specific frequency,²² impedance measurement,²³ slip-mode frequency shift,^{22,23} active frequency drift (AFD),^{5,24-26} Sandia voltage shift,²⁷ negative sequence current injection,²⁴⁻²⁸ high frequency signal injection,^{29,30} PLL perturbation and virtual capacitor.³¹ These active

detection methods are mostly used for inverter-based DERs. Active techniques decrease the non-detection zone (NDZ) and its error detection rate is also small.⁴ However, it needs additional equipment to inject perturbations into the system, which makes it complex. The injected perturbations further disturb the power quality of the system.

Passive islanding detection techniques are based on continuous monitoring of system parameters (voltage, frequency, active/reactive power) at point of common coupling (PCC) where utility, DER, and load are connected. The values of these parameters are analyzed with respect to a threshold value to decide either islanding has occurred or not. Passive techniques are suitable for practical implementation due to their cost-effectiveness and good power quality, but the main issue is their large NDZ. Hybrid techniques utilized the features of both passive and active techniques and present good performance with small NDZ as compare to passive techniques However, power quality issues still occur in it. Further demerits include large detection time and high cost. Voltage and real power shift, hybrid SMS and Q-f islanding techniques are examples of hybrid techniques.³²⁻³⁴

2. Discussion of Previous Work

Passive islanding detection techniques are commonly used by utility companies due to their low cost and very small impact on power quality as compared to other detection techniques.²⁸ It has been observed that most of the passive techniques rely on any one of the following parameters to distinguish islanding events from a non-islanding eventsa such as a change in a phase shift, change in harmonic impedance, rate of change of output power, and change in frequency.^{1,28} It is obvious that passive techniques that relied on a single parameter are less accurate and will possess a large non-detection zone (NDZ). Literature indicates that passive techniques depending on more than one parameter will be more accurate and their non-detection zone (NDZ) will also be small. It has been inferred that passive techniques based on two or more parameters are more accurate and show small NDZ in comparison to passive techniques based on a single parameter.³⁵

The change in the rate of output power and frequency, voltage unbalance and total harmonic distortion in current are an example of passive

The system as shown in Figure 2 is also modelled in a standard test frame (Figure 3) according to IEEE 1547-2003 standard to verify the performance of the presented technique.

4. Analysis for Sensitive Indices Selection

Simulations were executed to check the performance analysis of power system indices such as active power (P), reactive power (R), voltages (V), current (I), and all other selected parameters normally used by researchers. Table 1 shows the detail of the selected indices.

In this work, 12 power system indices were selected and tested under different islanding and abnormal conditions like capacitor injection/ ejection, increment/ decrement of load, single and three phase faults and induction motor starting conditions at different power mismatch levels between generation and load as displayed in Table 2.

The performance analysis of these power system indices is presented in Figure 4. All these values are taken in per unit (p.u). The P, Q, V, I, p.f, THD-V, and THD-I

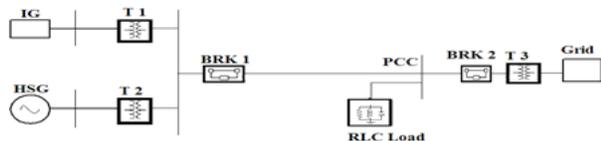


Figure 3. IEEE 1457 recommended test frame.

Table 1. Parameters (indices) used for sensitivity analysis

No.	Passive parameters
1.	Active power (P)
2.	Reactive power (R)
3.	Voltage (V)
4.	Current (I)
5.	Power factor (p.f)
6.	Phase difference (p.d)
7.	Total harmonic distortion of voltage (THD-V)
8.	Total harmonic distortion of current (THD-I)
9.	Voltage over power factor (v/p.f)
10.	Voltage times power factor (v*p.f)
11.	Frequency (f)
12.	Frequency over active power (f/P)

Table 2. Test cases

Testing case	Supply from grid		Supply from DERs	
	P (Grid) MW	Q (Grid) Mvar	P (DER) MW	Q (DER) Mvar
Islanding	0.5	0.5	4	2
	1	1	4	2
	1.5	1.5	4	2
	2	2	4	2
Faults	0.5	0.5	4	2
	1	1	4	2
	1.5	1.5	4	2
	2	2	4	2
Load switching	0.5	0.5	4	2
	1	1	4	2
	1.5	1.5	4	2
	2	2	4	2
Capacitor switching	0.5	0.5	4	2
	1	1	4	2
	1.5	1.5	4	2
	2	2	4	2

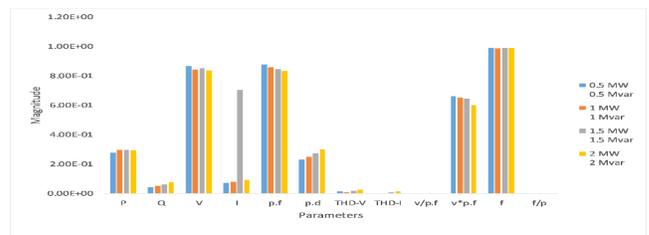


Figure 4. Islanding case.

express noteworthy changes during islanding condition as shown in Figure 4. However, it becomes difficult to distinguish between islanding and non-islanding events when these results are compared with the results of non-islanding conditions as displayed in Figures 5–10.

Among all these power system indices, only active power (P) has expressed a remarkable difference for both islanding and non-islanding cases. Thus, active power (P) is used for further analysis.

5. Methodology

After observing the performance capability of 12 distinct power system indices, it has been concluded that index active power is the most significant parameter to sense islanding. Therefore, an active power-based passive technique is recommended. The generalized procedure

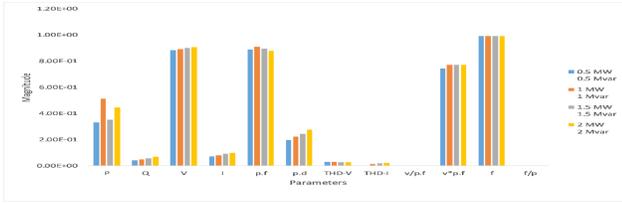


Figure 5. Capacitor switching (injection).

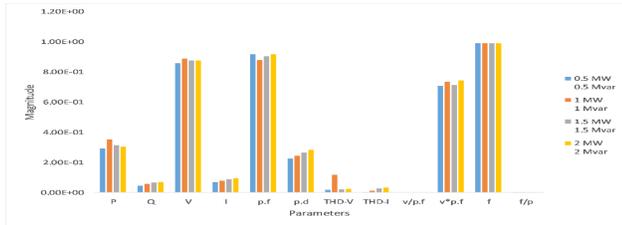


Figure 6. Capacitor switching (withdrawal).

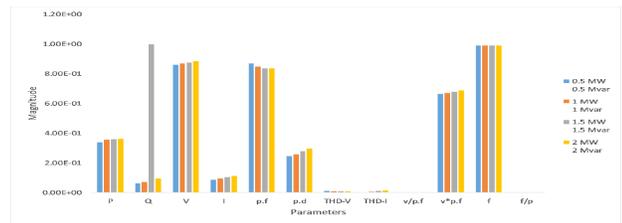


Figure 7. Load switching (increment).

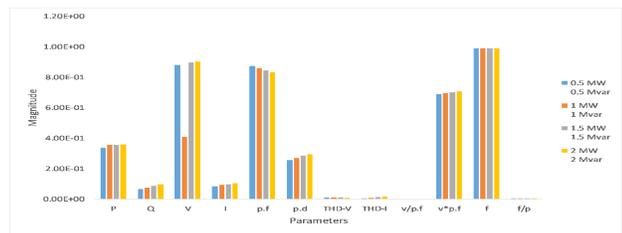


Figure 8. Load switching (decrement).

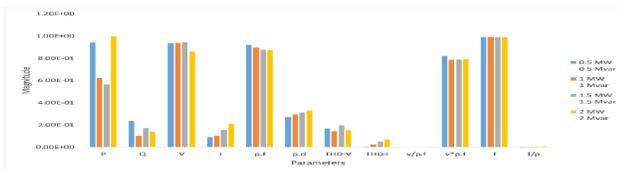


Figure 9. Single phase fault condition.

of this proposed technique is to take the mean of 5 maximum peaks of active power P at every 0.1 seconds. This technique starts working when Eq. (1) fulfills

$$P_{mean} < P_{threshold} \tag{1}$$

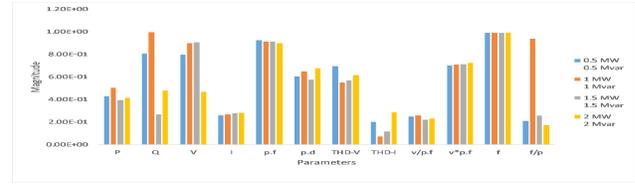


Figure 10. Three phase fault condition.

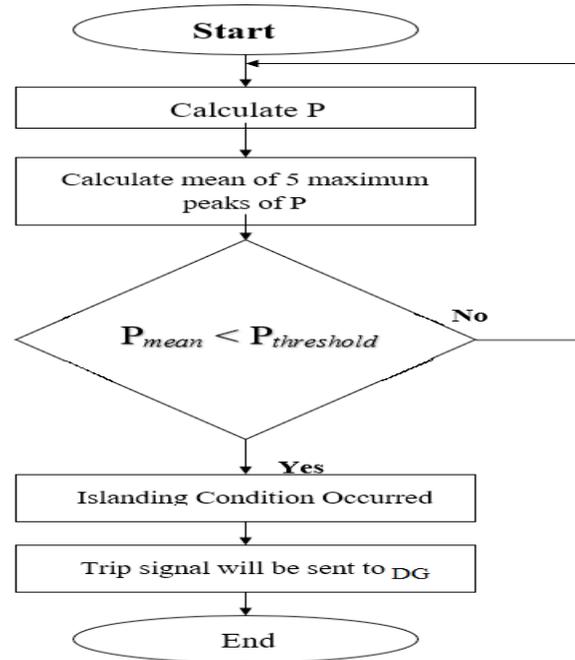


Figure 11. Proposed methodology.

where $P_{threshold}$ is the threshold value to differentiate islanding from all other non-islanding events. $P_{threshold}$ is identified from the analysis which was done in section 3. Moreover, this value is associated with specific systems, thus, it can be adjusted according to the system specification. The methodology for this technique is described in the following flow chart presented in Figure 11.

6. Results

The IEEE 1547 standard test system elaborated in Figure 2 is utilized to confirm the proposed islanding detection technique. All likely islanding and non-islanding scenarios are performed at 12 seconds, after the stabilization of the system. After the observation of the behavior of active power (P) under diverse islanding and non-islanding conditions, a threshold value of P is selected. A selected

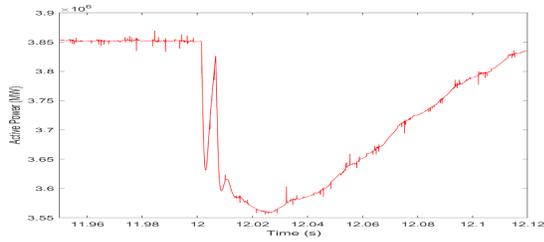


Figure 12. Close power mismatch scenario.

threshold value of P ($P_{threshold}$) for this system is 4.8 MW. The mean of 5 highest peaks of P is determined during the interval 12 to 12.10 seconds.

6.1. Islanding Under Close Mismatch Condition

In this situation, the DERs supply power of 3.84MW and 1.31 MVar, while the utility grid is supplying trivial power of 0.031 MW and 0.63 MVar to energize the load of 4 MW and 2.2 MVar.

The effect of the islanding state can be seen from Figure 12 and it has been inferred after analyzing that mean of 5 maximum peaks of P during 12 to 12.1 seconds interval, is 3.86 MW which is less than a selected threshold value. So, this proposed islanding technique precisely senses the islanding under close power mismatch and sends a tripping signal to disconnect the circuit breaker of DERs.

6.2. Islanding Under Large Mismatch Condition

In this condition, the power mismatch between the DERs and the load is 1.0 MW and 1.0 MVar. The DERs supplies a load of 3.84 MW and 1.31 MVar, while the remaining load is energized by the utility, resulting in a total load of 4.84 MW and 2.31 MVar. The effect of the islanding state can be seen from Figure 13 and it has been inferred after analyzing that mean of 5 maximum peaks of P during 12 to 12.1 seconds interval, is 4.72 MW which is less than a selected threshold value. So, this proposed islanding technique precisely recognize the islanding under large power mismatch and sends a tripping signal to disconnect the circuit breaker of DERs.

6.3. Load Increment and Decrement Condition

In this event, load increment and decrement of 0.6 MW and 0.6 MVar is applied. The effect of this load

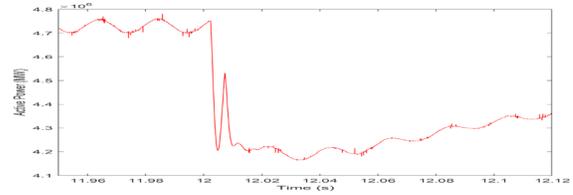


Figure 13. Large power mismatch scenario.

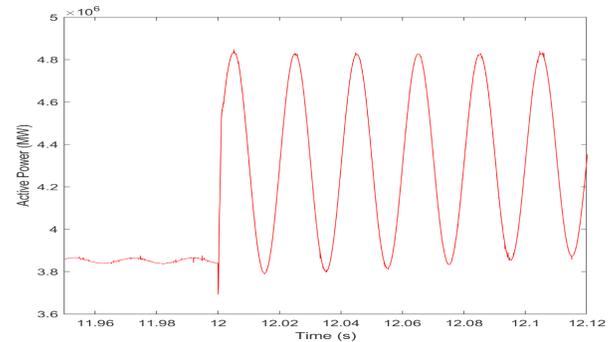


Figure 14. Load increment scenario.

increment and decrement can be observed in Figure 14 and Figure 15 respectively and it has been inferred after analyzing that mean of 5 maximum peaks of P during 12 to 12.1 seconds interval, for load increment is 4.85 MW and for load decrement is 4.82 MW. These values are greater than the threshold values. So, this recommended technique will detect this situation as a non-islanding event and no trip signal will be passed to the circuit breaker of DERs, and the system will keep working normally.

6.4. Capacitor Switching Condition

In this scenario, injection and ejection of the capacitor bank of 0.7 MVar are applied at the system, to validate the performance of the proposed technique for leading power factor cases. The effect of capacitor bank injection and ejection can be seen from Figures 16 and 17 respectively and it has been inferred after analyzing that mean of 5 maximum peaks of P during 12 to 12.1 seconds interval, for capacitor bank injection is 5.40 MW and it is 4.85 MW for capacitor bank ejection. These values are greater than the threshold values. So, this recommended technique will detect this situation as a non-islanding event and no trip signal will be passed to the circuit breaker of DERs, and the system will keep functioning normally.

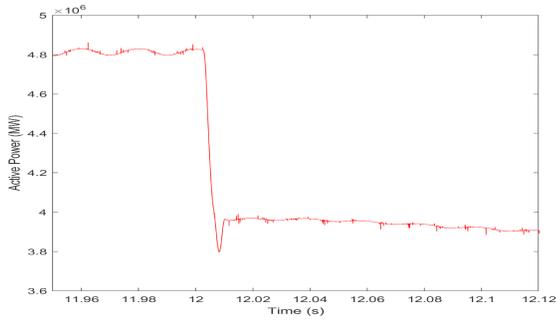


Figure 15. Load decrement scenario.

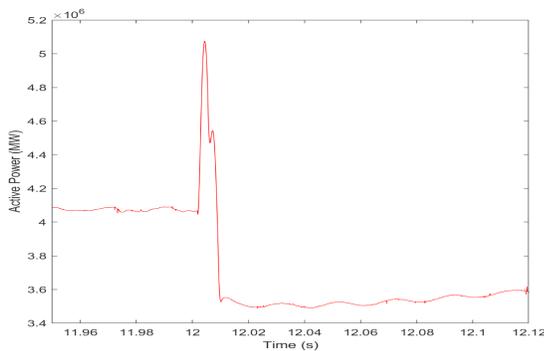


Figure 16. Capacitor injection scenario.

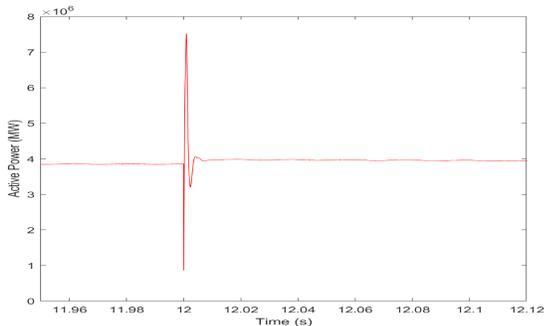


Figure 17. Capacitor ejection scenario.

6.5. Single and Three phase Scenarios

In this scenario, to validate the performance of the recommended technique, single and three phase faults were introduced in the system and duration for these instant faults was 0.01 second. The effect of single phase and three phase faults can be observed from Figures 18 and 19 respectively and it has been inferred after analyzing that mean of 5 maximum peaks of P during 12 to 12.1

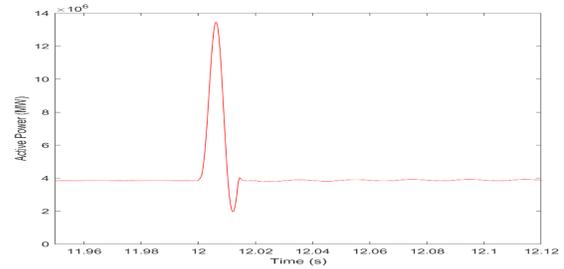


Figure 18. Single phase fault scenario.

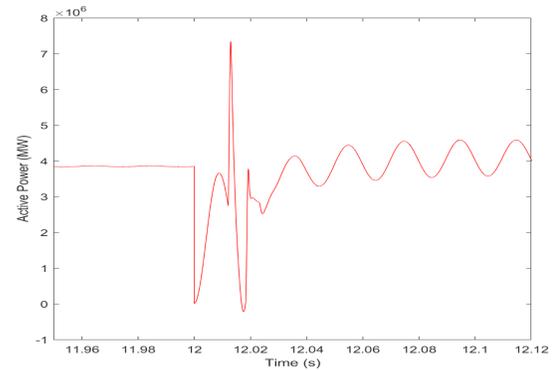


Figure 19. Three phase fault scenario.

seconds interval, for single phase the fault is 5.92 MW and for three phase the fault is 5.13 MW.

These values are greater than the threshold values. So, this recommended technique will detect this situation as a non-islanding event and no trip signal will be passed to the circuit breaker of DERs, and the system will keep working normally.

6.6. Induction Motor Starting

Induction motor possesses a very low power factor in its starting, so this aspect has a severe impact on power system performance. Hence, a 50 hp induction motor is inserted in the system to check the efficiency of the proposed technique. The impact of the insertion of induction motor in the system can be seen from Figure 20 and it has been inferred after analyzing that mean of 5 maximum peaks of P during 12 to 12.1 seconds interval, for the induction motor is 14.2 MW. This value is greater than the threshold value. So, this recommended technique will detect this situation as non-islanding event and no trip signal will be passed to the circuit breaker of DERs, and the system will keep working normally

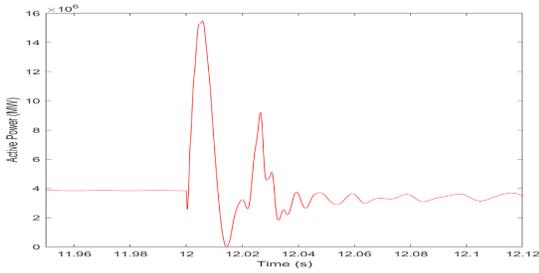


Figure 20. Induction motor start scenario.

7. Comparison with Conventional Detection Technique

This proposed passive technique is compared with the normally used voltage-based technique. All the simulation results for both islanding and non-islanding events are given in Table 3. It has been inferred from these results that traditionally practiced technique is unable to differentiate the islanding events from the non-islanding events appropriately for this system. Therefore, the threshold selection is quite complicated. In comparison to it, the proposed technique easily discriminates the islanding signatures from that of non-islanding signatures.

8. Non-detection Zone (NDZ)

NDZ is a key factor in the determination of the efficiency of an islanding technique. It is the region where the islanding technique cannot work properly. NDZ for active power is determined according to Eq. (2).^{42,43}

$$\Delta P = -3V \times \Delta V \times I \times \cos\phi \quad (2)$$

here, the active power imbalance is represented by ΔP , whereas I and V represent rated current and voltage, respectively. Moreover, deviation in voltage and power factor are represented by ΔV and $\cos\phi$ respectively. The highest and lowest voltage limits used for this system are 1.1 p.u and 0.9 p.u, respectively. So, for this system voltage deviation (ΔV) for the highest and lowest limits are 0.1 and -0.1 . The NDZ region for active power imbalance (ΔP) for this system is $+0.40$ MW and -0.40 MW. For reactive power, NDZ is determined by Eq. (3).^{42,43}

$$\Delta Q = \frac{3V^2}{\omega_n L} \left(1 - \frac{f_n^2}{(f_n \pm \Delta f)^2} \right) \quad (3)$$

Table 3. Comparison of proposed technique with normally used technique

Case	Scenario	P (MW)	Voltage (kV)
Islanding	Close power mismatch	3.86	6.20
	Large power mismatch	4.72	6.15
Non-islanding	Load increment	4.85	6.10
	Load decrement	4.82	6.30
	Capacitor injection	5.40	6.32
	Capacitor ejection	4.85	6.37
	Single phase fault	5.92	6.84
	Three phase fault	5.13	4.72
	Start of induction motor	14.2	4.52

Where, f_n is nominal frequency and f_Δ is the frequency deviation and $W_n = 2 \times \pi \times f$. The acceptable frequency deviation for this system is between -0.5 Hz to 0.5 Hz. So, NDZ for this system with respect to reactive power imbalance is 0.61 MVar and -0.63 MVar, respectively. After analyzing the simulation results, it has been inferred that this recommended technique works effectively when the active power imbalance is 0.013 MW and reactive power imbalance is 0.60 MVar.

Thus, as compared to other conventional techniques such as Over/Under frequency and Over/Under voltage,⁴⁴ this recommended technique shows increased accuracy and reduced NDZ.

9. Conclusion and Future Work

This study presents a new passive technique based on parameter index active power (P). This index-based parameter is selected after the evaluation of twelve different indices of the power system, based on sensitivity and precision. The performance and accuracy of the recommended technique are verified and tested against the distribution system which was modelled on the IEEE 1547 standard test system for different islanding and non-islanding events. This recommended technique can differentiate islanding events from a non-islanding events at a very small power mismatch of 0.013 MW and 0.60 MVar.

The major advantage associated with this technique is that it presents high accuracy and zero impact on power quality. These characteristics make this technique

appropriate for real-world operation. However, the drawback of this technique is the selection of threshold value and the presence of NDZ. These issues can be overcome by employing data mining techniques, which will be considered in future work. Furthermore, the in-depth characteristics of power system indices can be further studied under signal processing based techniques.

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